1. INTRODUCTION

Vibration-based electromagnetic harvester (VBEH) converts vibration energy into electrical energy. VBEHs are based on the phenomenon of resonance and narrow band of the excitation frequency. The VBEHs are reliable, simple in manufacturing, require small or no maintenance, and are available in sizes as small as micro-level. The energy harvesters find applications in the field of health monitoring, embedded sensors in aerospace, etc. In the last few decades, the researchers have developed electromagnetic harvesters using some innovative approaches such as providing a dynamic magnifier in the conventional electromagnetic harvester, or using multi-harvesters, etc. The harvested output powers of these VBEHs are of the order of a few microwatts.

Therefore, in this work, the focus is on the maximization of the output power of a VBEH required to sustain the electrical loads. To achieve this objective, one has to use the concept of impedance matching between VBEH and electrical load to investigate the effect of parameters involved in the electromechanical coupling. While optimizing the electromagnetic harvester output power, it is necessary to have the value of mechanical damping ratio \( \zeta_m \) much higher than that of the electrical damping ratio \( \zeta_e \). For this purpose, a VBEH is developed, which consists of the mechanical sub-system formed by a spring-mass-damper and an electromagnetic sub-system having a magnet and coil (in-line architecture) with the shunted electrical load. To obtain a high open-circuit voltage from the harvester, a hollow circular electrical coil is developed using a 41 gauge wire with 7790 number of turns and a NdFeB grade cylindrical magnet of 10 mm diameter and 30 mm height. The experimental setup is developed with the necessary instrumentation to carry out the following studies.

i) Determination of the values of electrical damping ratio \( \zeta_e \) and mechanical damping ratio \( \zeta_m \).
ii) the effect of variation of electrical impedance on the output power of the harvester.

2. LITERATURE REVIEW

William and Yates [1], in their work, represented the combination of mechanical and electrical damping as equivalent to viscous damping. William et al. [2] and Roundy et al. [3] have developed different types of prototype devices of vibration-based electromagnetic harvesters. Stephen [4,5] has analyzed the problem of the extraction of energy from a vibrating environment for both direct mass and base excitation. Their work shows that a highly damped system would extract energy over a wide bandwidth of the frequencies. The possible behavior of an adaptive device designed to operate within the available amplitude environment was also considered. The transfer of maximum power within electrical, mechanical, and electromechanical systems was studied. Spreemann et al. [6] developed an analytical expression for the magnetic field of a cylindrical permanent magnet used in VBEH. The realistic performance of the VBEH, in terms of output voltage, output power, and availability, was studied. Ooi et al. [7], in their work, have discussed a method of changing the value of
electrical damping in a vibration cycle to enhance the operational bandwidth of a VBEH. Szabo et al. [8], Nafair et al. [9] have discussed various methods of converting one form of energy to another. They designed a VBEH based on different coupling architectures operating in the low frequencies of excitation (0 to 100 HZ). Halim et al. [10,11] have shown that the electrical damping ratio may be adjusted by varying the resistive load to achieve the maximum power output. The damping characteristics of the electromagnetic harvester system are determined by using an impulse response. Zhang et al. [12] investigated the effect of ohmic resistors, rectifiers, and capacitors on electromagnetic harvested performance. They showed that the electromagnetic harvester performance using pure resistive load could not be generalized in all applications. Tai and Zuo [13] carried out the optimization for a maximum power of a VBEH through electrical load or electrical damping ratio and excitation frequency using two variable optimization analysis. Their work showed that the optimal electrical damping ratio is always larger than the mechanical damping ratio. Caruso [14] analyzed the electromagnetic harvester shunted to a resonant electric circuit, under harmonic excitation. Their work showed that a constant level of the harvester power can be achieved, under resonant excitation. Ashraf et al. [15] through their findings presented the method of improved energy harvesting from low-frequency vibrations and showed that the resonance amplification at multiple frequencies can improve the efficiency of harvesting energy from broadband vibrations. Simeone et al. [16] proposed a new strategy to obtain maximum power from an electromagnetic energy harvester by adjusting the electrical load according to the input level at the steady-state condition. They also showed that if the electrical load is tuned according to the level of harmonic excitation, then the harvester can always operate at the optimum conditions. Zuo and Cui [17] discussed about the dual-functional energy harvesting and vibration control. In their work, the viscous damping element between the tuned mass damper and the primary system is replaced by an electromagnetic transducer shunted to a resonant RLC Circuit. Using this concept, they showed that the vibration of the primary system can be minimized and the harvested electrical power maximized. Liu et al. [18] have derived ready to use analytical tuning laws for energy harvesting series electromagnetic tuned mass dampers. The numerical analysis showed that such a system can achieve enhanced performance in the form of both vibration control of the primary system and energy harvesting due to tuning of the resonance of the mechanical system and the electrical system. Tang and Zuo [19] in their work have showed that, theoretically, the energy harvesting can go to infinite value and state that a reasonably large electrical damping in dual-mass harvester can achieve more energy harvesting. Gilani [20] has developed a VBEH for an industrial centrifugal pump with a consideration that the VBEH will be an integral part of the autonomous vibration monitoring system. Tadesse et al. [21] have proposed and developed a multi-modal harvesting system or hybrid energy harvesting system to enhance the efficiency of mechanical energy harvesting and to improve the functionality of the electromagnetic harvesting system over the wide excitation frequency range. Bhatnagar and Owende [22] have presented the characteristics of common energy harvesting transducers and typical power density of ambient energy sources. Wang et al. [23-25] have reviewed available energy harvesting techniques that can be used for roadway and bridge for different applications and have given some suggestions for the research work in the area of energy harvesters. Zuo and Zhang [26] have presented a comprehensive assessment of the power that is available for harvesting in the vehicle suspension system. The road tests of the vehicle conducted to evaluate the energy potential and to verify the analytical results on vehicle suspension displacement, velocity, and energy. The effect of vehicle speed on harvested power is investigated. Chamanian et al. [27] have developed an electromagnetic energy harvester to be used in a wireless sensor node system for charging its rechargeable batteries while the system is operational. Yildrim et al. [28], El-Sayed et al. [29], carried out an extensive literature review covering the development in the design of VBEH and piezoelectric harvesters with various configurations and applications, and various techniques such as the use of a mechanical amplifier, multimodal arrays, etc., for enhancing the harvested power and widening of operation range. Malaji and Ali [30], Wang et al.[31], and Siang et al. [32] have carried out research studies on the methods of enhancing harvester output power, using different electrical coil and magnet system configurations.

This literature review reveals that only a few studies have been carried out on the effect of ohmic load or matched load on the power harvested from a VBEH. Hence, in this work, experimental studies are carried out to study the effect of various types of shunted electrical loads on the performance of a VBEH. Since the average generated power $P_{ave}$, depends predominantly on the electrical damping ratio $ζ_e$ and the value of $ζ_e$ is determined by transient open circuit response and the loaded impulse response of the developed VBEH. The value of $ζ_e$ is also calculated using the theoretical relation developed by Spreemann et al. [6].

### 3. VIBRATION BASED ELECTROMAGNETIC HARVESTER (VBEH)

The vibration-based electromagnetic harvester as shown in Fig. 1, is a single degree of freedom (SDOF) system consisting of mass ($m$), spring ($k$), and damper ($c$) subjected to sinusoidal base excitation $y(t)$. In this system: $c = cm + ce$ where $cm$ = mechanical damping coefficient and $ce$ = electrical damping coefficient.

![Figure 1: Schematic of Single Degree of Freedom (SDOF) VBEH](image)

The displacement of harvester mass is $x(t)$. The relative displacement $z(t)$ between the mass and the base...
is \([x(t) - y(t)]\) and the base displacement \(y(t)\) is equal to \(Y\sin(\omega t)\), where \(\omega\) is the circular excitation frequency. The governing equation of the harvester system is:

\[
m\ddot{z} + c\dot{z} + kz = -m\dot{y}
\]

(1)

The average generated power \(P_{\text{ave}}\) from VBEH is calculated using Eq.(2) given by William et al. [1,2]

\[
P_{\text{ave}} = m^2\left(\frac{\omega}{\omega_n}\right)^3 \left[1 - \left(\frac{\omega}{\omega_n}\right)^2\right] + 2\left(\xi_e + \xi_m\right) \frac{\omega}{\omega_n}^2
\]

(2)

where, the electrical damping ratio \(\xi_e = \frac{c_e}{c_c}\), the mechanical damping ratio \(\xi_m = \frac{c_m}{c_c}\), the critical damping coefficient is \(c_c\), and circular natural frequency of a mechanical sub-system is \(\omega_n\).

4. EXPERIMENTAL SETUP: VBEH SHUNTED TO ELECTRICAL LOADS

In this section, the experimental setup developed for the measurement of average harvested power \(P_{\text{aveh}}\) from VBEH is described. Figure 2 shows a schematic VBEH shunted to an electrical load circuit composed of an inductance \(L\), resistance \(R_L\), and capacitance \(C\).

![Figure 2. Schematic of VBEH with shunted electrical load](image)

This schematic of VBEH is converted into an experimental setup. In this setup, the mechanical sub-system and electrical coil-magnet sub-system with magnet holding devices are as shown in Fig.3. Figure 4 shows the overall experimental setup of VBEH equipped with a mechanical sub-system and electrical sub-system shunted to a resonant electric circuit.

In the setup, a DC motor is mounted on the base frame. A Cam - follower system is placed on the shaft of the DC motor to convert rotary motion into simple harmonic motion. The amplitude of base excitation of 1mm is provided by adjusting the cam eccentricity, and the frequency of excitation varied by changing the speed of DC motor drive. The plate representing the mass ‘m’ moves, within linear bearings, between two parallel guide rods. The upper end of spring is connected to the mass plate, and the lower end of the spring is connected to the wooden support. The electrical coil is fixed on the wooden support, and the magnet is attached to the mass plate to obtain relative motion \(z(t)\) between the coil and magnet. Displacement response of the harvester mass is measured by using the ultrasonic displacement sensor, and a proximity speed sensor measures the speed of the DC drive motor. These sensors are connected to a computer through an Arduino device to get the records of the response.

![Figure 3. Overall Experimental Setup](image)

4.1 Design of electrical coil-magnet system (in-line architecture)

A cylindrical magnet moves in an electrical coil in the direction of motion, as shown in Fig. 5.

![Figure 5. Magnet and coil (in-line configuration)](image)
[33], the total number of turns $N_{total}$ comes out to be 7790, and the copper fill factor $k_{co}$ as 0.06522. The number of longitudinal turns $N_{long}$ and the number of lateral turns $N_{lat}$ are as 342 and 22.80, respectively.

Figure 6. Developed coil

The resistance of the coil $R_c$ is determined using Eq. (3) [11]:

$$R_c = \frac{4\rho\left(\frac{r_0^2 - r_1^2}{a}\right)h_{coil}}{a^2} = 1814\Omega$$

where $\rho$ is the specific resistivity of the copper wire material = $1.72 \times 10^{-8}$, $\Omega m$ and $a$ is the cross-sectional area of wire = $8.04 \times 10^{-9} m^2$. However, the measured value of $R_c$ was found to be 1620 $\Omega$. The difference between the theoretical and experimental value of the internal resistance of the coil may be due to the coil winding method and calculating the number of turns of the coil. With this value of $R_c$, the final specifications of the developed coil are as shown in Table 1

Table 1. Specifications of the developed coil

<table>
<thead>
<tr>
<th></th>
<th>Outer radius of the coil (mm)</th>
<th>11</th>
</tr>
</thead>
<tbody>
<tr>
<td>$r_i$</td>
<td>Inner radius of the coil (mm)</td>
<td>8</td>
</tr>
<tr>
<td>$h_{coil}$</td>
<td>Height of coil (mm)</td>
<td>30</td>
</tr>
<tr>
<td>$N_{long}$</td>
<td>Number of Longitudinal turns</td>
<td>343</td>
</tr>
<tr>
<td>$N_{lat}$</td>
<td>Number of Lateral turns</td>
<td>23</td>
</tr>
<tr>
<td>$N_{total}$</td>
<td>Total number of turns</td>
<td>7790</td>
</tr>
<tr>
<td>$R_c$</td>
<td>The resistance of the coil ((\Omega))</td>
<td>1620</td>
</tr>
<tr>
<td>$L$</td>
<td>The inductance of coil (H)</td>
<td>0.45</td>
</tr>
</tbody>
</table>

4.2 Selection of magnet

Alnico, ceramic (hard ferrite), samarium cobalt, and neodymium iron boron NdFeB are the four types of available magnetic materials. Neodymium Iron Boron (NdFeB) magnet is composed of rare earth magnetic material with a high coercive force and strength, and is relatively low cost, and easy to machine. Hence, a cylindrical magnet of 10 mm diameter and 30 mm height of NdFeB grade 30 material was selected for the electrical coil sub-system.

5. EXPERIMENTAL ANALYSIS

This analysis carried out, to study the effect of various types of shunted electrical loads on the performance of a VBEH

5.1 Frequency response curves (with and without coil magnet system)

Using the experimental setup in Fig. 4, the frequency response curves for the mechanical sub-system are obtained using an ultrasonic sensor for the measurement of the relative displacement between mass $m$ and the base at various values of angular excitation frequency $\omega$ in the range of 18 to 21.0 rad/sec, shown in Fig. 7.

Figure 7. Relative amplitude $Z$ vs. Excitation frequency $\omega$

Figure 7 shows that the relative amplitude $Z$ is maximum at the resonant frequency for both with and without a coil magnet system as it is expected.

5.2 Open Circuit Voltage $E$ Generated Across the Coil

Figure 8 shows the graph of open-circuit voltage $E$ vs. excitation frequency $\omega$.

The peak voltage, at resonance, recorded across the coil is found to be 9 $V$.

6. EFFECT OF SHUNTED ELECTRICAL LOADS ON AVERAGE HARVESTED POWER $P_{AVEH}$

For matched electrical $R_{L}-L-C$ load circuit of VBEH, the undamped circular natural frequency $\omega_n$ of electrical load, a circuit is made equal to the undamped circular natural frequency $\omega_n$ of the mechanical sub-system.

$$\omega_n = \frac{1}{\sqrt{LC}}$$, $\omega_n = 19.05$ rad/sec and $\omega = \omega_n$. With value of $L = 0.45H$, the value of $C$ is calculated as 0.006123 F (6123 $\mu F$). The values of $L$ and $C$ varied around these values.

6.1 Voltage $V_R$ across the resistive load $R_L$

The resistive load $R_L$ connected across the coil is varied as 500 $\Omega$, 1000$\Omega$, 1500$\Omega$, 2000$\Omega$, 3000$\Omega$ and 4000$\Omega$. The voltage $V_R$ across $R_L$ measured is by a Digital Storage Oscilloscope (DSO). From Fig.9, it is seen that for an increase in $R_L$ value by 8 times, the increase in $V_R$ is approximately 3 times.
6.2 Average harvested power $P_{aveh}$ at various values of resistive load $R_L$

From Fig. 10 it is seen that the value of $P_{aveh}$ is again maximum at resonance and at $R_L = 1600 \, \Omega$ and $P_{aveh}$ is minimum at 500 $\Omega$.

$$\text{Figure 9. } V_R \text{ vs. Resistive Load } R_L \text{ at } \omega = \omega_n$$

$$\text{Figure 10. } P_{aveh} \text{ vs. Resistive Load } R_L \text{ at } \omega = \omega_n$$

6.3 Voltage $V_R$ across the various combined values of resistive load and inductive load

Figure 11 shows the combined resistive and inductive electrical load circuit of VBEH. In this case, the load impedance $Z_1$ due to shunted electrical load (combined resistive and inductive load) given by:

$$Z_1 = \sqrt{R_L^2 + x_L^2}$$

where $R_L$ is the resistive load and inductance reactance $x_L = \omega L$. Figure 12 shows the variable inductance coil.

$$\text{Figure 11. Electrical load circuit}$$

$$\text{Figure 12. Variable Inductance coil}$$

The values of $V_R$ measured are plotted at different values of $Z_1$ by varying the excitation frequency.

$$\text{Figure 13. } V_R \text{ vs. Load Impedance } Z_1 \text{ at } \omega = \omega_n$$

$$\text{Figure 14. } P_{aveh} \text{ vs. Load Impedance } Z_1 \text{ at } \omega = \omega_n$$

6.4 Average harvested power $P_{aveh}$ at various values of resistive load and inductive load.

Figure 13 shows the curve of peak values of $V_R$ vs. $Z_1$, and Fig 14 shows the curve of values of $P_{aveh}$ vs. $Z_1$ at resonance, respectively.

6.5. Voltage $V_R$ across the various combined values of resistive load $R_L$, inductive load, and capacitive load.

Figure 15 shows the combined resistive, inductive, and capacitive electrical load circuit of the VBEH. In this case, the load impedance $Z_2$ due to shunted electrical load (combined resistive, inductive, and capacitive load) given by:

$$Z_2 = \sqrt{R_L^2 + x_L^2 + x_C^2}$$

where, $R_L$ is the resistive load, inductance reactance $x_L = \omega L$, and capacitive reactance $x_C = \frac{1}{\omega C}$, where $C$ is capacitance. The values of load impedance $Z_2$ for various values of resistive, inductive, and capacitive loads are tabulated in Table 3. Figures 16 (a) and 16 (b), show the variable inductance coil and capacitors, respectively.

Table 2. Values of load impedance $Z_1$ for various values of resistive and inductive loads for $\omega_L = \omega_n$

<table>
<thead>
<tr>
<th>Sr. No</th>
<th>Resistive Load $R_L$ ((\Omega))</th>
<th>Inductance $L$ ((H))</th>
<th>Reactance $x_L$ ((\Omega))</th>
<th>Load impedance $Z_1$ ((\Omega))</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>400</td>
<td>0.310</td>
<td>5.625</td>
<td>400.3</td>
</tr>
<tr>
<td>2</td>
<td>900</td>
<td>0.310</td>
<td>5.625</td>
<td>900.01</td>
</tr>
<tr>
<td>3</td>
<td>1600</td>
<td>0.510</td>
<td>9.608</td>
<td>1600</td>
</tr>
<tr>
<td>4</td>
<td>2100</td>
<td>0.510</td>
<td>9.608</td>
<td>2100.02</td>
</tr>
<tr>
<td>5</td>
<td>2800</td>
<td>0.700</td>
<td>13.188</td>
<td>2800.03</td>
</tr>
</tbody>
</table>

Table 3. Values of load impedance $Z_2$ for various values of resistive, inductive, and capacitive loads.

<table>
<thead>
<tr>
<th>Sr. No</th>
<th>Resistive Load $R_L$ ((\Omega))</th>
<th>Inductance $L$ ((H))</th>
<th>Reactance $x_L$ ((\Omega))</th>
<th>Reactance $x_C$ ((\Omega))</th>
<th>Load impedance $Z_2$ ((\Omega))</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>400</td>
<td>0.310</td>
<td>5.625</td>
<td>1/100</td>
<td>400.3</td>
</tr>
<tr>
<td>2</td>
<td>900</td>
<td>0.310</td>
<td>5.625</td>
<td>1/200</td>
<td>900.01</td>
</tr>
<tr>
<td>3</td>
<td>1600</td>
<td>0.510</td>
<td>9.608</td>
<td>1/300</td>
<td>1600</td>
</tr>
<tr>
<td>4</td>
<td>2100</td>
<td>0.510</td>
<td>9.608</td>
<td>1/400</td>
<td>2100.02</td>
</tr>
<tr>
<td>5</td>
<td>2800</td>
<td>0.700</td>
<td>13.188</td>
<td>1/500</td>
<td>2800.03</td>
</tr>
</tbody>
</table>
Table 3. Values of load impedance $Z_2$ for various values of resistive, inductive and capacitive loads for $\omega = \omega_n$

<table>
<thead>
<tr>
<th>Sr.</th>
<th>Resistive Load ($R_L$)</th>
<th>Inductance ($L$)</th>
<th>Capacitance ($C$)</th>
<th>Load impedance $Z_2$ ($\Omega$)</th>
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</thead>
<tbody>
<tr>
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<td>900.01</td>
</tr>
<tr>
<td>3</td>
<td>1600</td>
<td>0.510</td>
<td>0.0054</td>
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</tr>
<tr>
<td>4</td>
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<td>0.510</td>
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<tr>
<td>5</td>
<td>2800</td>
<td>0.700</td>
<td>0.0069</td>
<td>2800.03</td>
</tr>
</tbody>
</table>

Table 3 gives the values of load impedance $Z_2$. The curves of $V_R$ vs. excitation frequency $\omega$ for the various value of $Z_2$ plotted.

6.6 Average power harvested $P_{\text{aveh}}$ at different values of $Z_2$

The effect of varying the value of $Z_2$ (at resonance) on $V_R$ and $P_{\text{aveh}}$ are respectively shown in Fig. 17 and Fig. 18. Figure 17 reveals that $V_R$ is maximum (5.5V) at $Z_2 = 2800\,\Omega$ and Fig.18 reveals that $P_{\text{aveh}}$ is maximum (13.81mW) at $Z_2 = 1600\,\Omega$.

7. DISCUSSION OF RESULTS

The comparison of the results shown in figures 9, 13, and 17 for the voltage $V_R$ across the resistance of the value $R_L$, $Z_1$, and $Z_2$ shows that as the resistive load $R_L$ increases the voltage $V_R$, at resonance, increases quickly up to $R_L = 1600\,\Omega$, $Z_1 \approx 1600\,\Omega$ and $Z_2 \approx 1600\,\Omega$. For the various values $R_L$, $Z_1$, and $Z_2$ greater than 1600$\Omega$, the voltage increases steadily.

From the comparison of the results shown in the figures 10, 14, and 18, it can be seen that average power harvested $P_{\text{aveh}}$ is maximum at or near the value of $Z_1 \approx 1600\,\Omega$ and $Z_2 \approx 1600\,\Omega$. The effect of the addition of inductive and capacitive load is to widen the range of values of load impedances at which the maximum $P_{\text{aveh}}$ is obtained. Also, it is seen that the values of $V_R$ and $P_{\text{aveh}}$ are maximum at or near $R_L = 1600\,\Omega$ or $Z_1 \approx 1600\,\Omega$ or $Z_2 \approx 1600\,\Omega$ which is very close to the internal resistance of the coil of the electromagnetic sub-system.

7.1 Average generated power $p_{\text{ave}}$ from VBEH

Equation (2) of section 3 gives the average generated power $p_{\text{aveh}}$ from VBEH. In Eq. (2), $m$ is the harvester mass, $\omega$ is the excitation frequency, $\omega_n$ is the undamped circular natural frequency of the mechanical sub-system, $Y$ is the amplitude of excitation, $\zeta_m$ is the mechanical damping ratio, and $\zeta_e$ the electrical damping ratio.
Eq. (2) shows that $P_{ave}$ is controlled by $\zeta_e$, therefore, the experimental determination of $\zeta_e$ is carried out by the procedure outlined in the next section.

7.2 Experimental determination of $\zeta_m$

Using the experimental setup developed for VBEH (without electrical load), a transient response curve $E$ (open-circuit voltage) vs. time $t$, as shown in Fig. 19 is obtained using a digital storage oscilloscope (screenshot). From this curve, $\zeta_m$ was determined using the method of logarithmic decrement and is found to be 0.025.

7.2 Experimental determination of $\zeta_m$ (Method 1)

Using the experimental setup developed for VBEH (with an electrical resistive load of 1600 $\Omega$), a transient response curve $V_R$ (voltage across resistive load) vs. time $t$, as shown in Fig. 20, is obtained using a digital storage oscilloscope (screenshot). From this curve, using the method of logarithmic decrement, the total damping ratio $\zeta$ was determined and is found to be 0.03. Now, $\zeta = \zeta_m + \zeta_e$. With $\zeta_e = 0.03$ and $\zeta_m = 0.025$ from method 1, the electrical damping ratio $\zeta_e$ obtained as 0.005, and is denoted as $\zeta_{e1}$.

The electrical damping ratio calculated as [11]

$$\zeta_e = \frac{(N_{total}B_{L1})^2}{2m\omega_n (R_c + R_L)}$$  \hspace{1cm} (4)

In Eq. (4), $N_{total}$ is the total number of turns, $L_1$ is length of the coil, $m$ is mass, $\omega_n$ is circular natural frequency, $R_c$ is the resistance of the coil, $R_L$ is the resistive load, and $B$ is the magnetic flux density in the direction of the axis of the magnet. The value is calculated, as explained by Halim et al. [10]. The magnetic flux density $B$ is given by Eq. (5).

$$B = \frac{B_r}{2} \left[ \frac{h_{mag} + x}{\sqrt{R_{mag}^2 + (h_{mag} + x)^2}} - \frac{x}{\sqrt{R_{mag}^2 + x^2}} \right]$$  \hspace{1cm} (5)

At $x=0$, i.e. at the point near the magnet pole face, the value of $B$ is maximum. For the developed VBEH, a cylindrical NdFeB magnet of height $h_{mag}=0.03m$, radius $R_{mag}=0.005 m$, and having the residual magnetic flux density $B_r = 0.87T$ was selected. Substituting these values of $h_{mag}$, $R_r$, and $B_r$ in Eq. (5), the value of $B$ at pole face ($x=0$) is found to be 0.39T.

The value of $B$ is also determined using the standard Tesla meter setup, as shown in Fig. 21. Figure 22 shows the curves of experimental magnetic flux density $B$ vs. distance $x$ from the magnet pole face for the magnets measuring 4 mm and 5 mm in radius.

7.3 Determination of Electrical damping ratio $\zeta_e$ (Method 2)

The electrical damping ratio is obtained as [11]

$$\zeta_e = \frac{(N_{total}B_{L1})^2}{2m\omega_n (R_c + R_L)}$$  \hspace{1cm} (4)

The plot of $P_{ave}$ vs. $\omega$ is, obtained and is as shown in Fig. 23. Substituting the values $m = 4.31 kg$, $\omega_n = 19.05$ rad/sec, $\zeta_m = 0.025$, $Y = 0.001 m$ and $\zeta_e = \zeta_{e1} = 0.005$ in Eq. (2), and varying the excitation frequency $\omega$ in the range of 17.50 to 20.50 rad/sec.

7.4 Average Generated Power $P_{ave}$ from the developed VBEH.

The experimental value of $B$ for 10mm diameter NdFeB magnet is obtained as 0.44T. The value of $B$ obtained from Eq. (05) is in close agreement with that obtained from experimental measurement. Using the values $B = 0.44T$, $N = 7790$, $L_1 = 0.019 m$, $m = 4.31 kg$, $\omega_n = 10.05$ rad/sec, $R_c = 1620 \Omega$, and $R_L=1600 \Omega$ in Eq. (4), the value of $\zeta_e$ from method 2 is obtained as 0.008, and is denoted as $\zeta_{e2}$.

The analytical expression for the electrical damping factor $\zeta_e$ is obtained by equating the power dissipation in the coil and shunted electrical load impedance to that obtained from the electromagnetic force. The electrical damping ratio $\zeta_e$ is obtained as $\zeta_e = \frac{C_e}{2m\omega_n}$.

From the expression for the $\zeta_e$ in Eq. 4, it can be seen that for the given coil magnet configuration, size, and for the value of natural frequency of the mechanical sub-system (tuned to excitation frequency of the ambient vibration) the value of $\zeta_e$ is dominated by the value of load resistance. Thus as the shunted electrical load increases the value of $\zeta_e$ decreases, and the value of total damping ratio $\zeta$ decreases, resulting in more harvested power from VBEH.
The average harvested power $P_{aveh}$ is maximum at the resonant frequency, for the resistive load of 1600Ω. The average harvested power $P_{aveh}$ is much less than the average generated power $P_{ave}$. The value of electrical damping ratio $\zeta_e=0.005$, (method 1) is less than that obtained using the analytical formula for $\zeta_e$ (0.008), for the resistive and inductive load. The values of the average generated power $P_{ave}$ and average harvested power $P_{aveh}$ of VBEH are maximum when the value of excitation frequency equals the natural frequency of the mechanical sub-system of the VBEH. These results bring out the importance of the experimental determination of the electrical damping ratio in the maximization of the output power of the VBEH shunted to electrical loads.

8. CONCLUSIONS

From the results obtained from the experiments and mathematical equations, the following conclusions are drawn.

1. The effect of variation of shunted electrical loads $R_L$ (resistive), $Z_L$ (resistive and inductive) and $Z_L$ (resistive, inductive and capacitive) on the average harvested power $P_{aveh}$ is maximum at resonance. The $P_{aveh}$ decreases with an increase in electrical load on the harvester. It shows that the value of $P_{aveh}$ is maximum at the resistive load of 1600Ω. This research work is in line with the research results reported in the state-of-the-art of the design and development of vibration-based energy harvesters.

2. Using the transient response curve of open-circuit voltage $V(t)$ vs. time $t$, the mechanical damping ratio $\zeta_{me}$ is estimated as 0.025, and Using the transient response curve of $V_R(t)$ vs. time $t$, total damping ratio $\zeta$ is determined as 0.03, at the resistive load of 1600Ω. From the estimated values of $\zeta$ and $\zeta_{me}$, the electrical damping ratio $\zeta_e$ was calculated as $\zeta_e = \zeta - \zeta_{me} = 0.005$, (method 1 of section 7.2) . Also the value $\zeta_e = 2\zeta_{me} = 0.008$ was estimated using the analytical formula for $\zeta_e$ [11]. It shows that the value of electrical damping ratio $\zeta_e$ is very small as compared to the value of mechanical damping ratio $\zeta_m$ (0.025). This is desirable to obtain maximum harvester power from a VBEH. This result will undoubtedly be beneficial in the design and development of vibration-based energy harvesters.

3. The value of the average generated power $P_{ave}$ based on the electrical damping ratio $\zeta_e$ (method 1) is less than that obtained using the analytical formula for $\zeta_e$ (method 2). The average generated power $P_{ave}$ is maximum, at the resonant frequency, for the resistive load of 1600Ω. The average harvested power $P_{aveh}$ is much less than the average generated power $P_{ave}$.

DECLARATION OF CONFLICT OF INTEREST

The author(s) declared no potential conflict of interest in regard to the research, authorship and/or publication of this article.

FUNDING INFORMATION

The author(s) received no financial support for the study, authorship, and publication of this article.

REFERENCES


NOMENCLATURE

<table>
<thead>
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<th>Symbol</th>
<th>Description</th>
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<tbody>
<tr>
<td>N</td>
<td>Speed rpm</td>
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<tr>
<td>z</td>
<td>Relative displacement of mass w.r.t.base</td>
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<tr>
<td>ż</td>
<td>Relative velocity of mass w.r.t.base</td>
</tr>
<tr>
<td>z̈</td>
<td>Relative acceleration of mass w.r.t.base</td>
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<tr>
<td>ω</td>
<td>Circular excitation frequency, rad/sec</td>
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<tr>
<td>ωn</td>
<td>Circular natural frequency rad/sec</td>
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<tr>
<td>ωω</td>
<td>Frequency ratio</td>
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<tr>
<td>m</td>
<td>Mass, Kg</td>
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<tr>
<td>K</td>
<td>Spring rate, N/m</td>
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<tr>
<td>cm</td>
<td>Mechanical damping coefficient</td>
</tr>
<tr>
<td>ce</td>
<td>Electrical damping coefficient</td>
</tr>
<tr>
<td>c</td>
<td>Damping coefficient c= cm + ce</td>
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<tr>
<td>ζm</td>
<td>Mechanical Damping ratio.</td>
</tr>
<tr>
<td>ζe</td>
<td>Electrical damping ratio.</td>
</tr>
<tr>
<td>ζ</td>
<td>Damping ratio = ζm + ζe</td>
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<tr>
<td>X</td>
<td>Displacement amplitude of mass, m</td>
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<tr>
<td>Y</td>
<td>Amplitude base excitation, m</td>
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<tr>
<td>Z</td>
<td>Relative amplitude(X-Y), m</td>
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<tr>
<td>Z1</td>
<td>Load Impedance, Ω</td>
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<tr>
<td>Z2</td>
<td>Impedance load, Ω</td>
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<tr>
<td>E</td>
<td>Open circuit Voltage, V</td>
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<tr>
<td>Vr</td>
<td>Voltage across the load resistance, V</td>
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<tr>
<td>Pave</td>
<td>Average generated Power, mW</td>
</tr>
<tr>
<td>Paveh</td>
<td>Average harvested Power, mW</td>
</tr>
<tr>
<td>ωe</td>
<td>Circular natural frequency of the electrical circuit, rad/sec</td>
</tr>
<tr>
<td>B</td>
<td>Magnetic flux density, T</td>
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<tr>
<td>B_r</td>
<td>Residual magnetic flux density ,T</td>
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<tr>
<td>h_mag</td>
<td>Height of magnet, m</td>
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<tr>
<td>R_mag</td>
<td>Radius of the magnet m</td>
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<td>x</td>
<td>Distance from magnet pole face, m</td>
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<tr>
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<tr>
<td>L</td>
<td>Inductive load H</td>
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<tr>
<td>C</td>
<td>Capacitive load F</td>
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ЕКСПЕРИМЕНТАЛНО ИСТРАЖИВАЊЕ УТИЦАЈА ПАРАЛЕЛНИХ ЕЛЕКТРИЧНИХ ОПТЕРЕЂЕЊА НА ПЕРФОРМАНСЕ ЕЛЕКТРОМАГНЕТНОГ САКУПЉАЧА ЕНЕРГИЈЕ БАЗИРАНОГ НА ВИБРАЦИЈАМА

В.Б. Патил, М. Сакри

Данас се истраживачи хватају у коштац са проблемима максимизирања излазне снаге код електромагнетног сакупљача енергије базираног на вибрацијама (ВВЕХ). Параметри који утичу на излазну снагу ВВЕХ-а су: однос електричног пригушења (ζ_e), однос механичког пригушења (ζ_m) и импеданса оптерећења паралелног електричног оптерећења. Зато је обављено експериментално истраживање утицаја паралелног електричног оптерећења на излазну снагу ВВЕХ-а и одређиване ζ-e који максимизира излазну снagu. ВВЕХ је дизајниран и развијен да би се добио висок напон отвореног кола. Утицај отпорног, индуктивног и капацитетног оптерећења на излазну снагу ВВЕХ-а је истражен помоћу експеримента постављеног за наведене параметре. Утврђено је да је излазна снага ВВЕХ-а максимална при резонантној фреквенцији, када је еквивалентна импеданса оптерећења једнака унутрашњем отпору електромагнетног калема и када је вредност ζ-e веома мала у односу на вредност ζ_m.